

# Subsurface probing of planetary bodies

*Marek Banaszkiewicz*  
*Space Research Centre PAS*

*in cooperation with: B. Dabrowski, J. Grygorczuk,  
K. Seweryn, R. Wawrzaszek*

# Outline

- Surface and subsurface thermal physics
- Missions with subsurface science
- Thermal sensors
- Models and measurements
- Heat transport in granular media

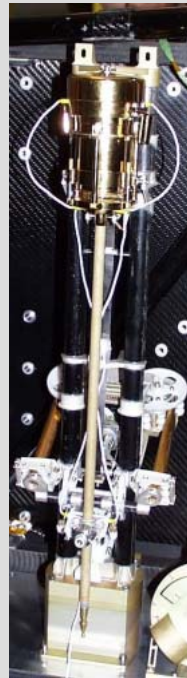
# Why to go under the surface

- To take samples and analyse their chemical & mineralogical composition
- To perform measurements of physical properties (seismometry, thermal properties, mechanical properties, structure)
- To reach deep layers of the body (subsurface ocean on Europa)
- To collect minerals and precious materials (e.g. He-3 on the Moon)

# Techniques of surface and subsurface exploration



Taking samples



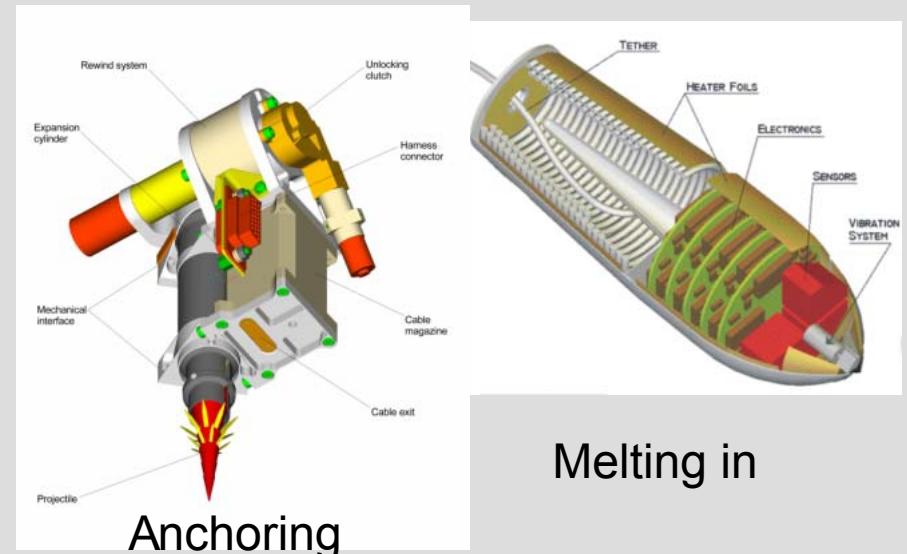
Hammering



Penetrating mole



Drilling



Anchoring

Melting in

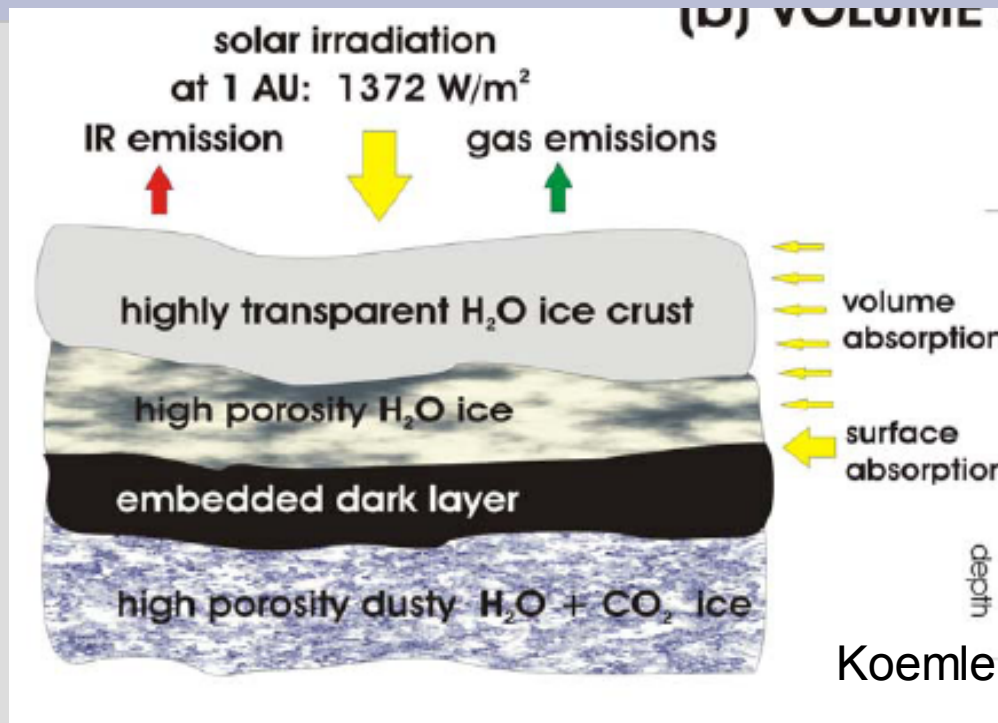
# Thermal processes in planetary bodies

- Heat sources
  - hot interior
  - surface irradiation
- Thermal transport processes
  - heat conduction (in solid, liquid and gas phases)
  - radiative transfer
  - advection/convection (mass motion)

## Quantities to be determined:

- Temperature profile  $T(z)$
- Heat flow  $K \nabla T$
- thermal conductivity  $K$ , thermal diffusivity, thermal inertia

# Example: heat transport in comets



Heat transport equation  
(Prialnik & Podolak)

Conduction

$$(\rho_a + \rho_c + \rho_s) \frac{\partial u(T)}{\partial t} + (\rho_d c_d + \rho_v c_v + \rho_g c_g) \frac{\partial T}{\partial t} + \nabla \cdot \mathbf{F} + (c_v J_v + c_g J_g) \cdot \nabla T = \lambda(T) \rho_a (1 - f_p) H_{\text{sc}} - q_v H_v - q_g H_g$$

Advection

Amorph. ice  
 $\rightleftharpoons$  cryst. ice

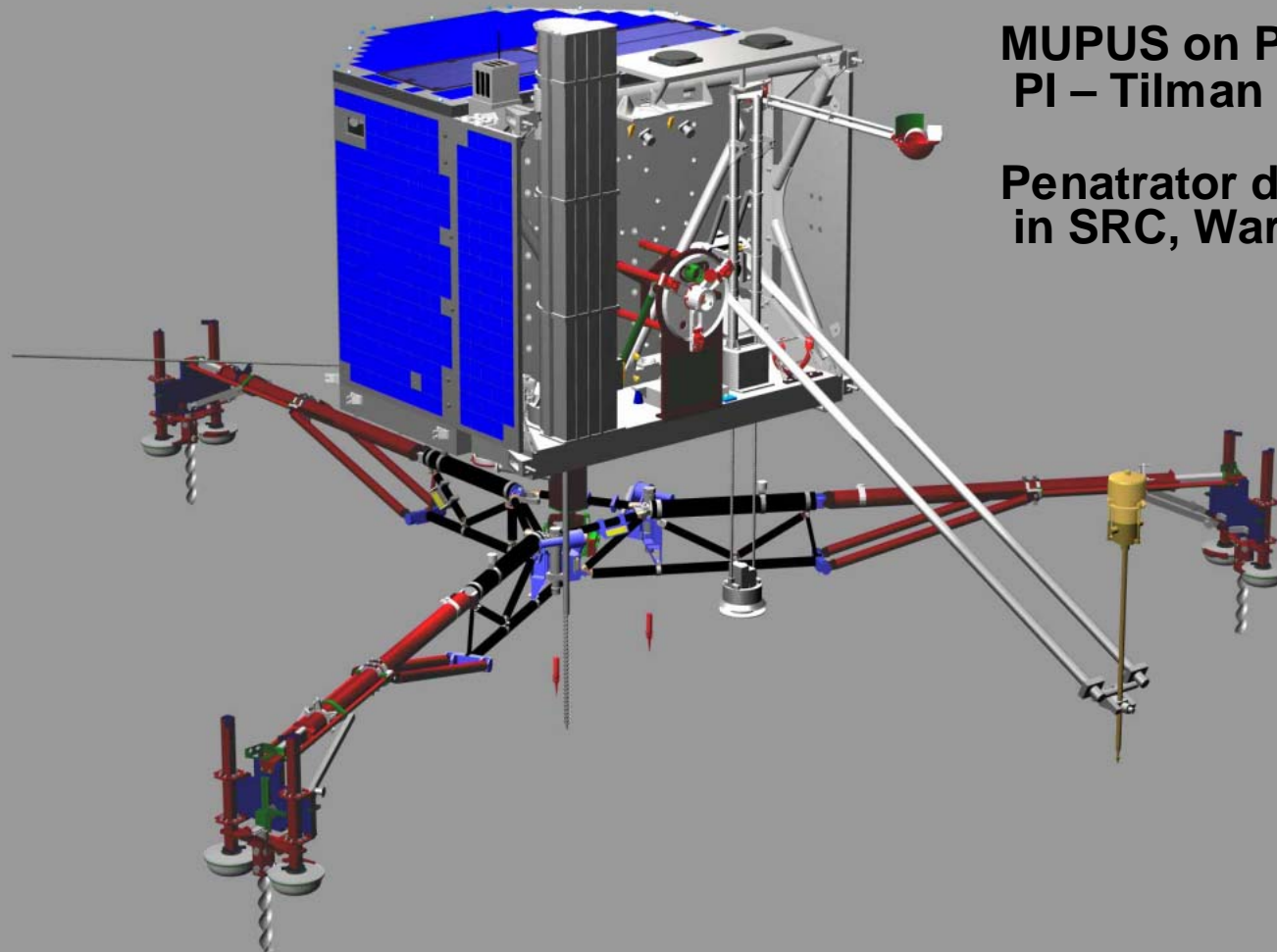
Sublimation

# Missions with subsurface thermal experiments

- Apollo 15 & 17
- Mars-Express: Beagle
- Rosetta: MUPUS (Philae)
- Phobos-Grund
- Exo-Mars: HP3

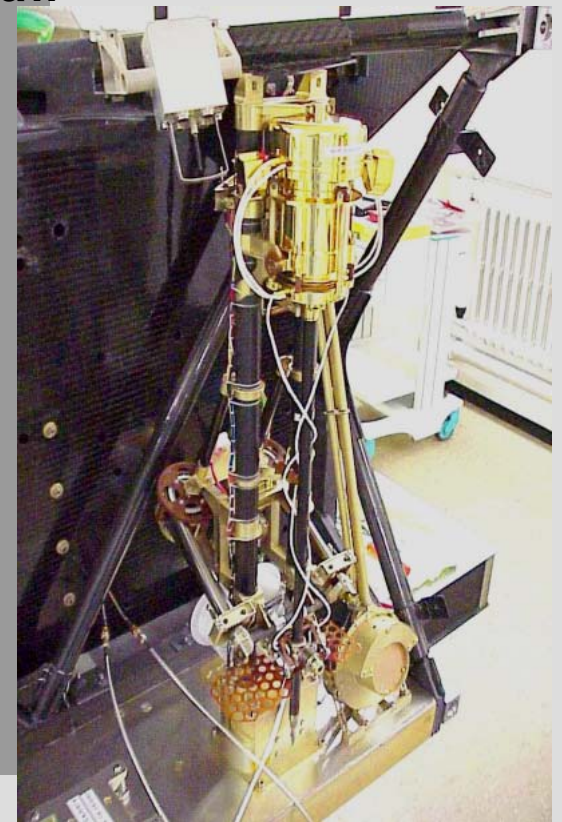
**Apollo:** thermal probes inserted into boreholes 2m deep, but sensors not properly deployed, therefore heat flow values, 28-33 mW / m<sup>2</sup> questioned => the uncertainty in the lunar core temperature is 250 - 400°

# Penetrators



**MUPUS on Philae (Rosetta Lander)  
PI – Tilman Spohn (DLR)**

**Penetrator designed & manufactured  
in SRC, Warsaw**





# Penetrators: moles

- HP3 (Exo-Mars) – Beagle heritage

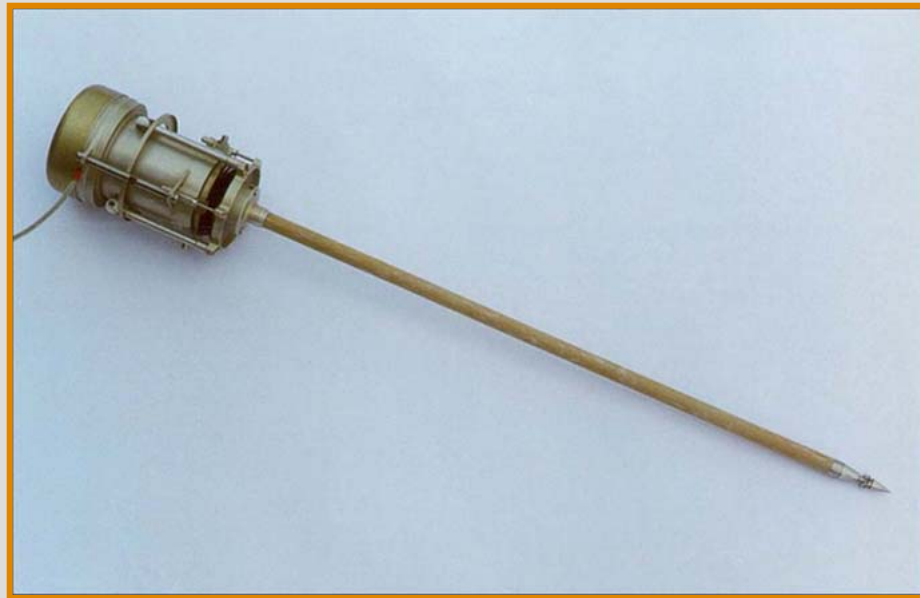


SRC  
Design



# Thermal sensors

- Resistance thermometers



## THP sensors

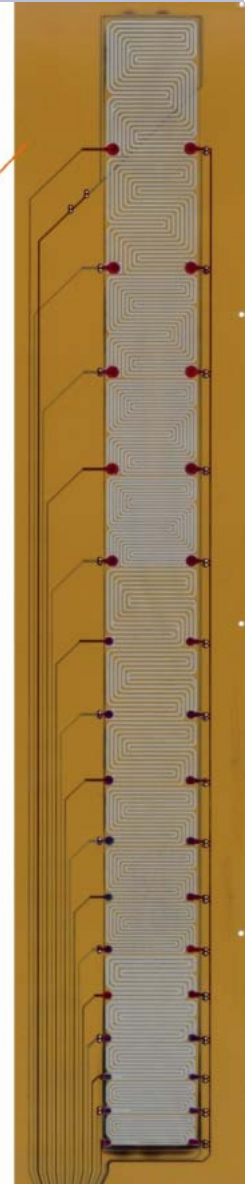
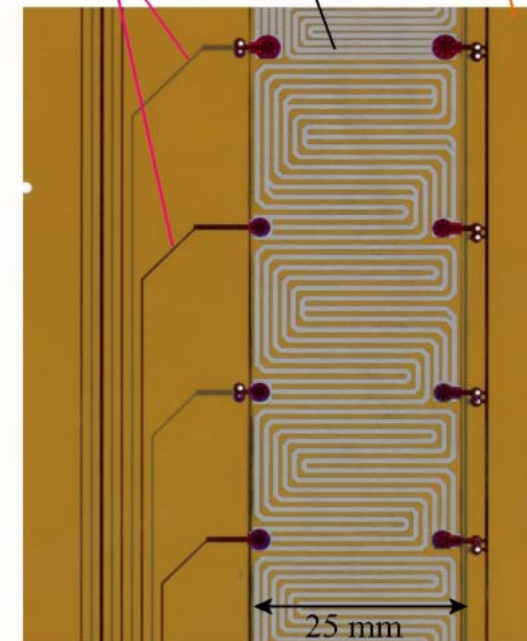
- design for MUPUS 1999

active area = 1  $\text{cm}^2$   
length = 325 mm

kapton  
50  $\mu\text{m}$  thick

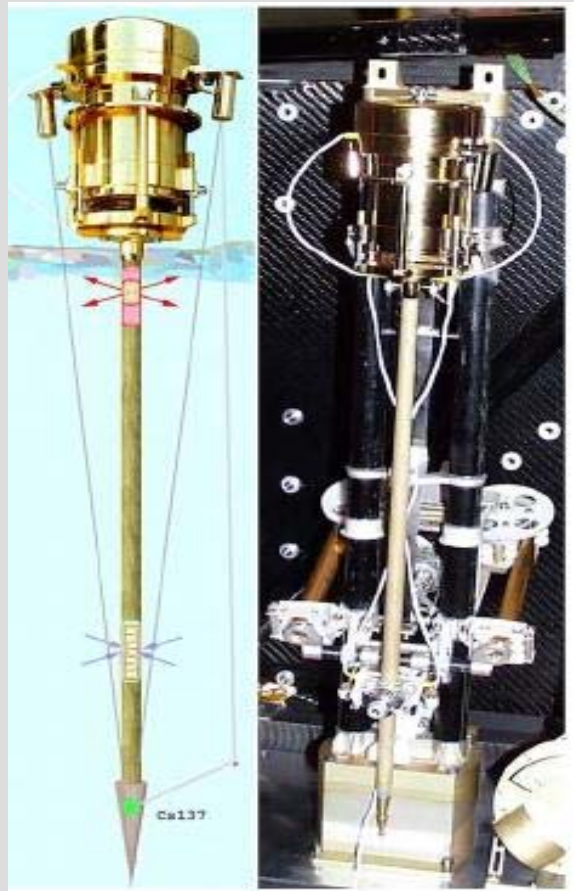
Titanium thin layer  
< 0.5  $\mu\text{m}$  thick

Copper paths  
17  $\mu\text{m}$  thick



# Thermal sensors

- Principle of operation



## Hot rod method

### Thermal conductivity measurements:

$$T - T_0 = \frac{2Q\alpha^2}{\pi^3\lambda} \int_0^\infty \frac{1 - \exp(-\kappa tu^2/r^2)}{u^3 \Delta(u, \alpha)} du$$

**Where:**

**t - time**

**$T_0$  - initial temperature**

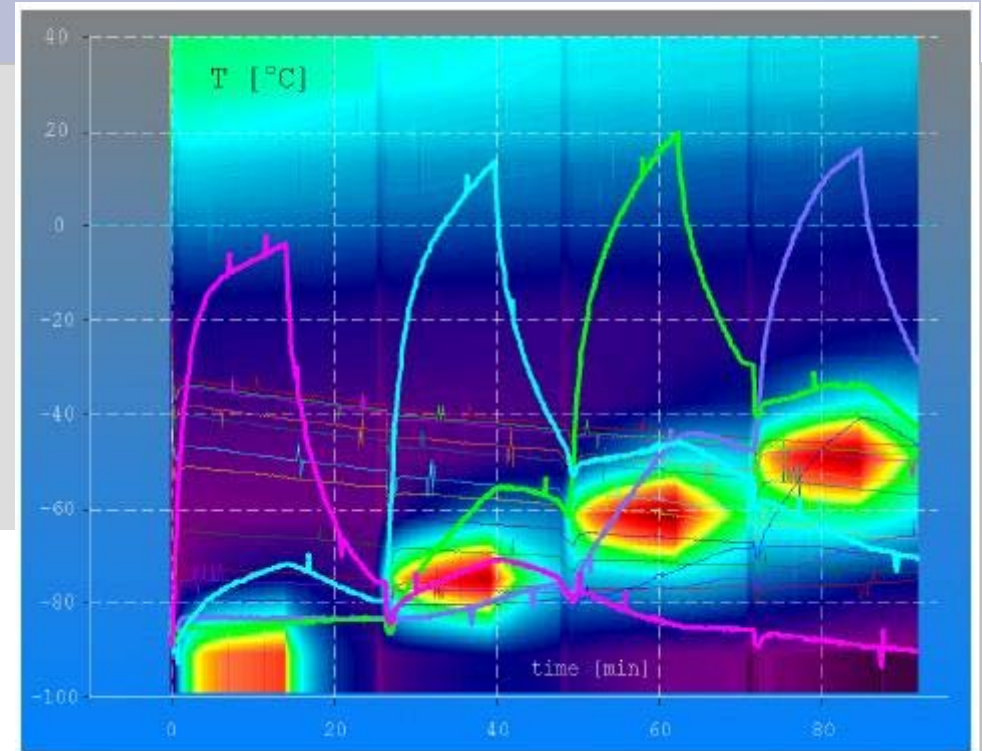
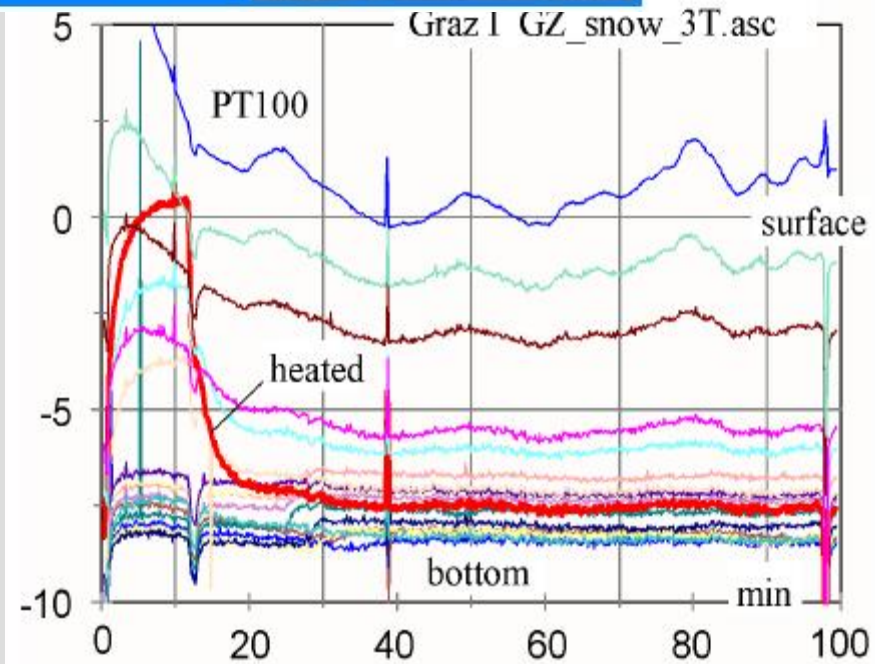
**Q - applied heating power**

**$\lambda$  - thermal conductivity**

**$\kappa$  - thermal capacity**

**$\alpha$  - heat capacity ration: medium to wire**

# MUPUS measurements on Earth

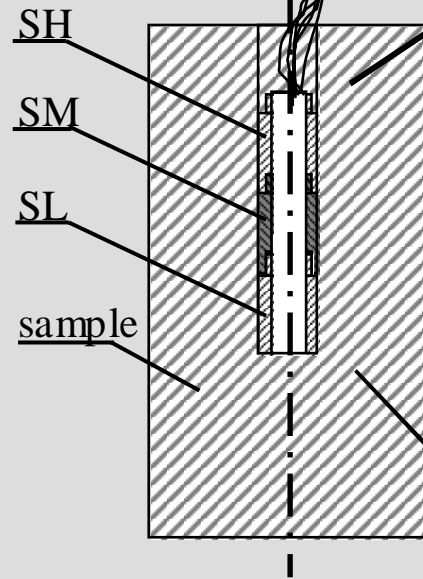


# Potential problems

- Conductivity of thin sensors (titanium, copper) is different than the conductivity of the bulk material
- Calibration: precise  $K(T)$  dependence should be taken
- Aging effects => recalibration 12 years after sensor manufacturing should be done
- Two wire method used => reference current should be measured before each measurement
- Heating and temperature measurements must be done sequentially

# New sensors

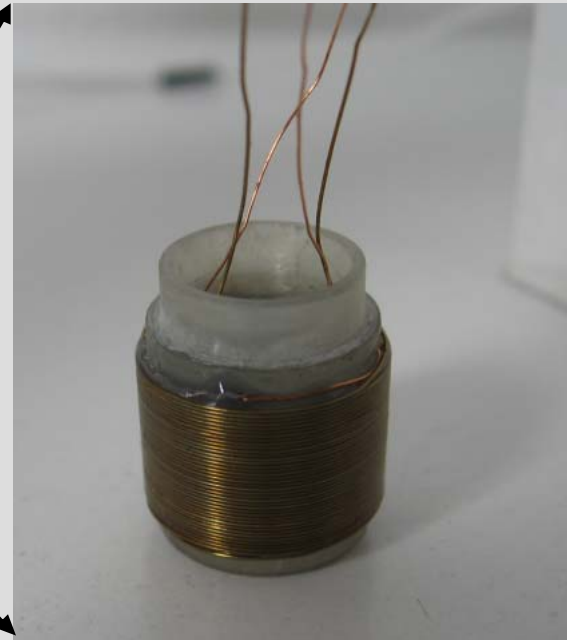
(wires to measure- and-  
power-supply system)



a)

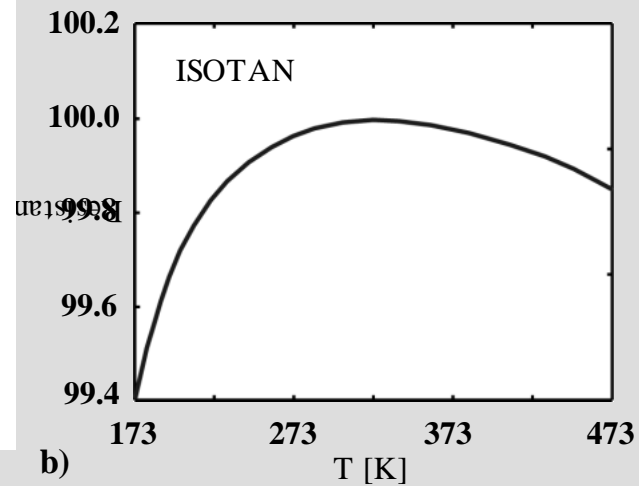
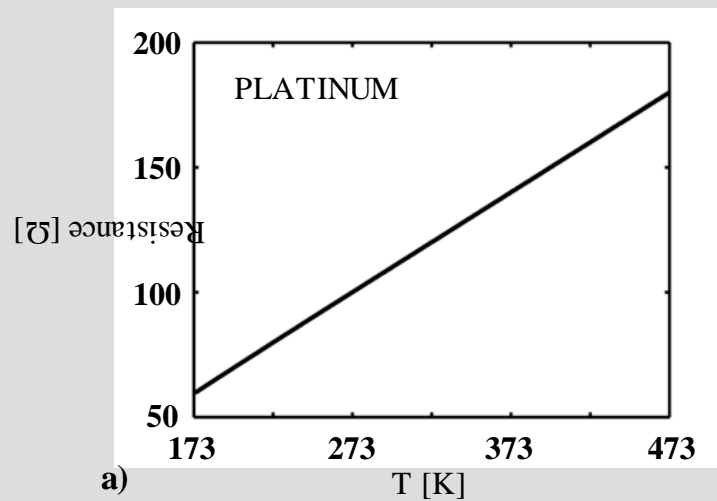
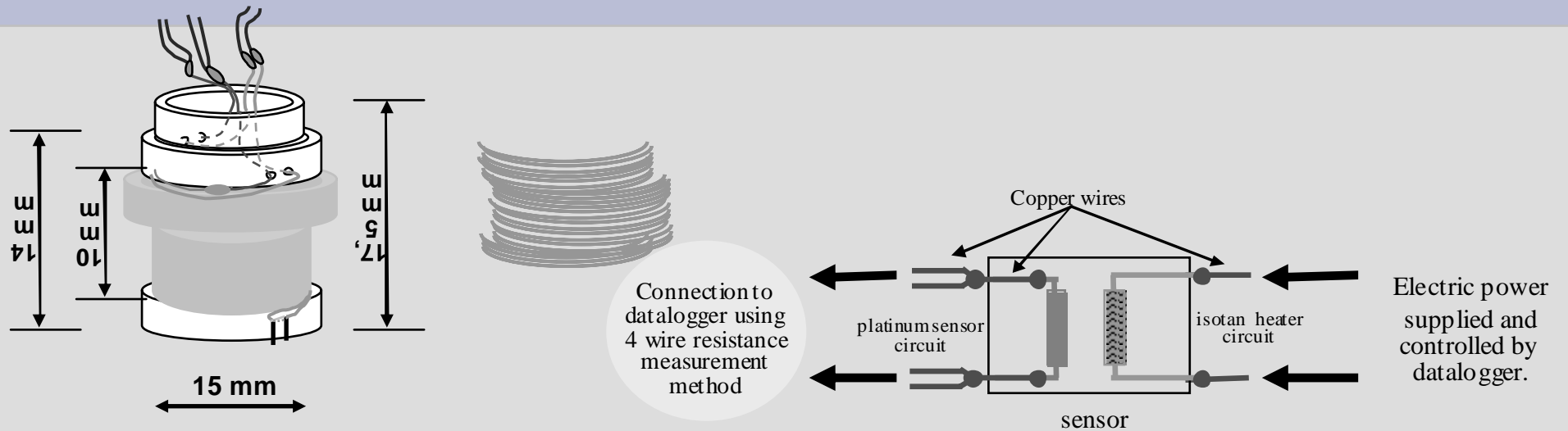


b)



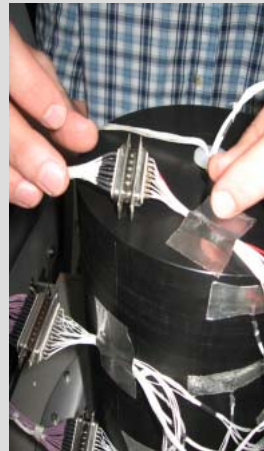
c)

# New sensors



# Thermal measurements

- Cometary material & asteroid regolith analogues
- Teflon and delrin as reference materials



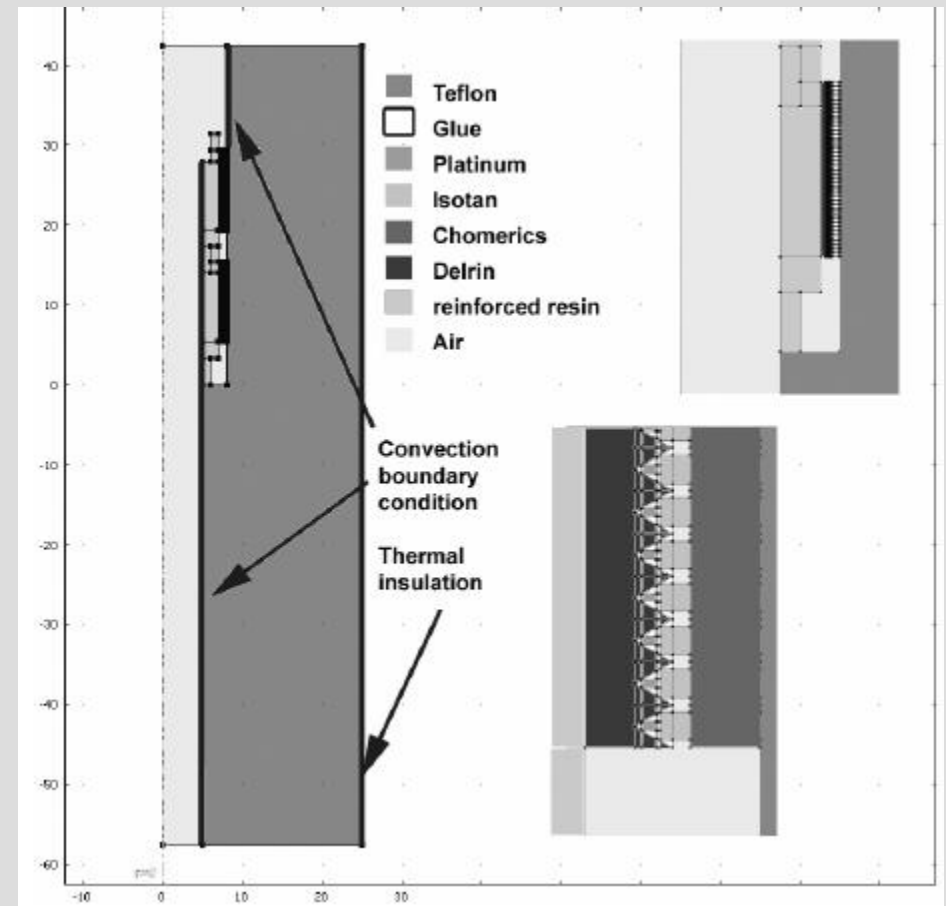
- Measurements in thermal and thermal-vacuum chambers



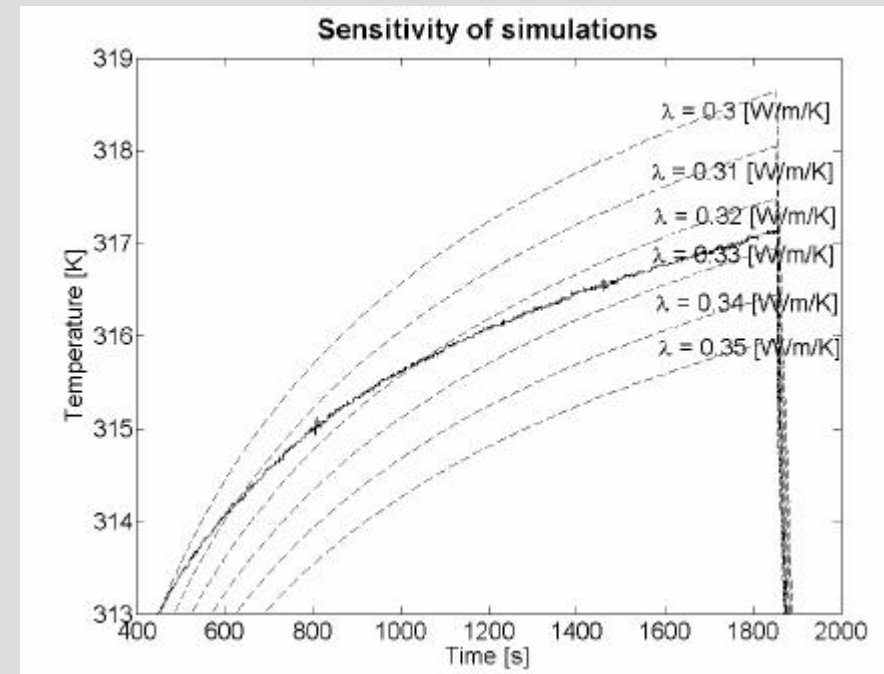
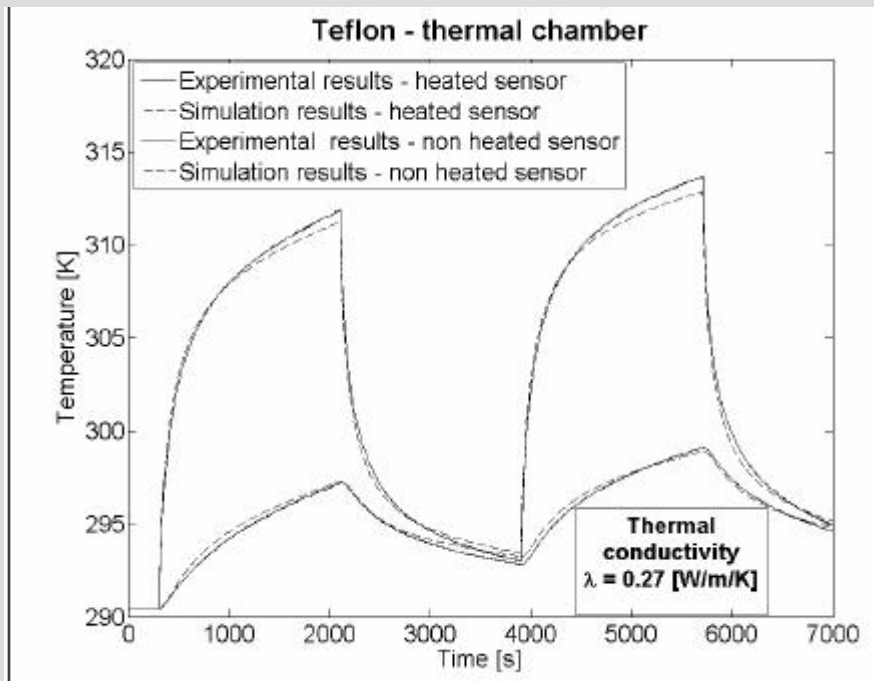


# Models

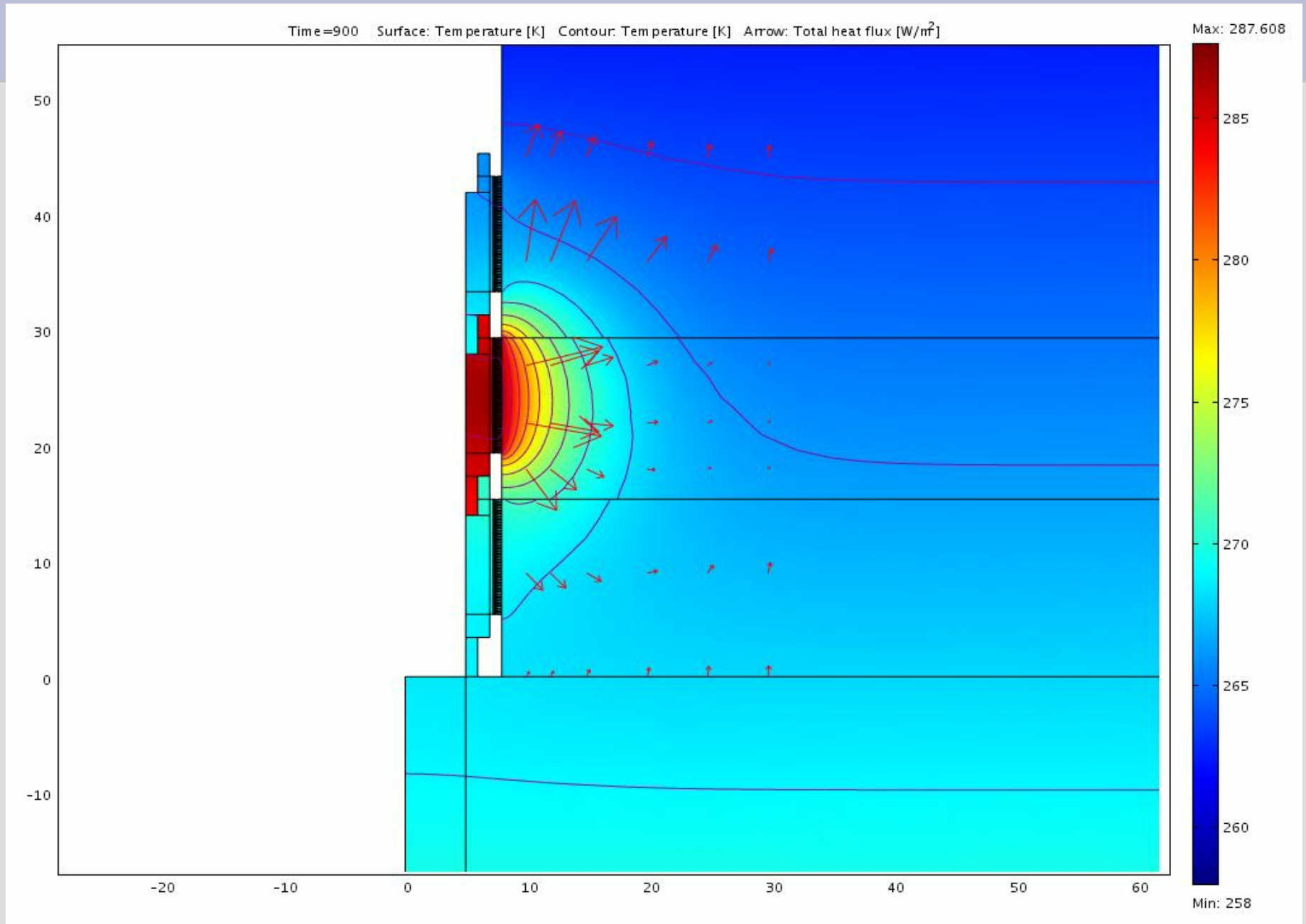
- Analytical: applicable for simple geometries and quite complicated
- Semi analytical based on Green functions
- Numerical: FEM



# Measurements: calibration

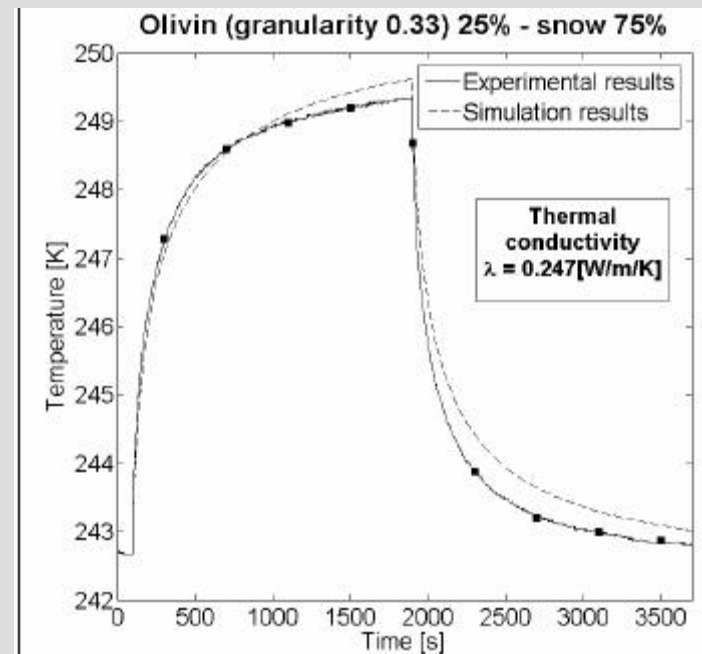
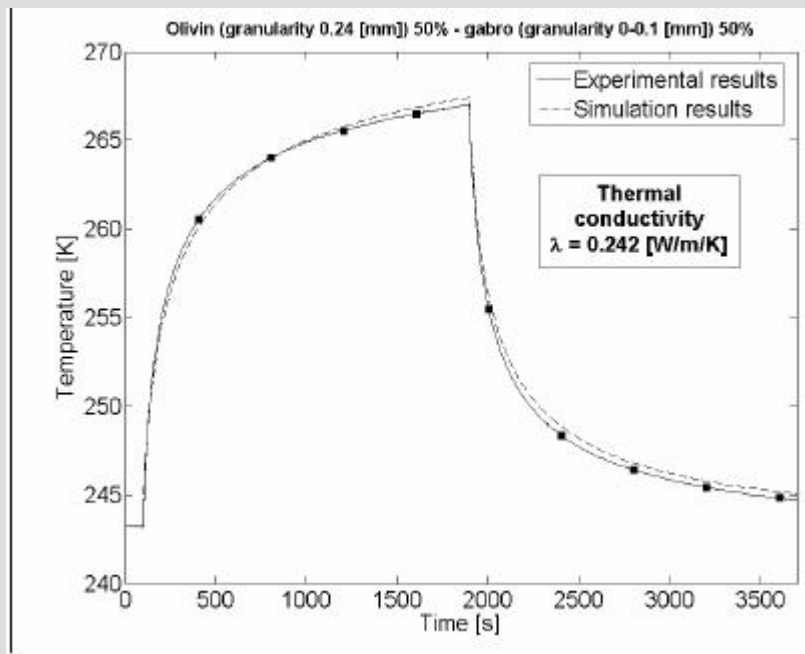


# Measurements



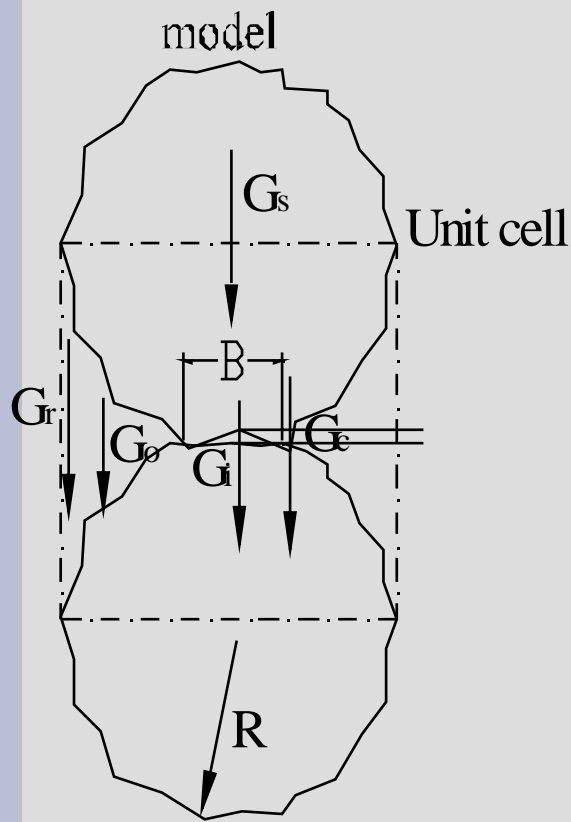
# Measurements

- In thermal chamber => K in the narrow range 0.2 -0.4 W/m/K



# Granular media

- Different transport processes (Slavin et al.)



$$\dot{Q} = K_{\text{eff}} 4R^2 \frac{(T_1 - T_2)}{2\alpha_c R} = G(T_1 - T_2)$$

$$G = G_r + \frac{G_s(G_{\text{par}})}{G_s + G_{\text{par}}} \text{ with } G_{\text{par}} = G_o + G_i + G_c.$$

$$G_s = K_s \alpha_s \pi R^2 / 2R, G_c = K_s \alpha_c \delta / h_r,$$

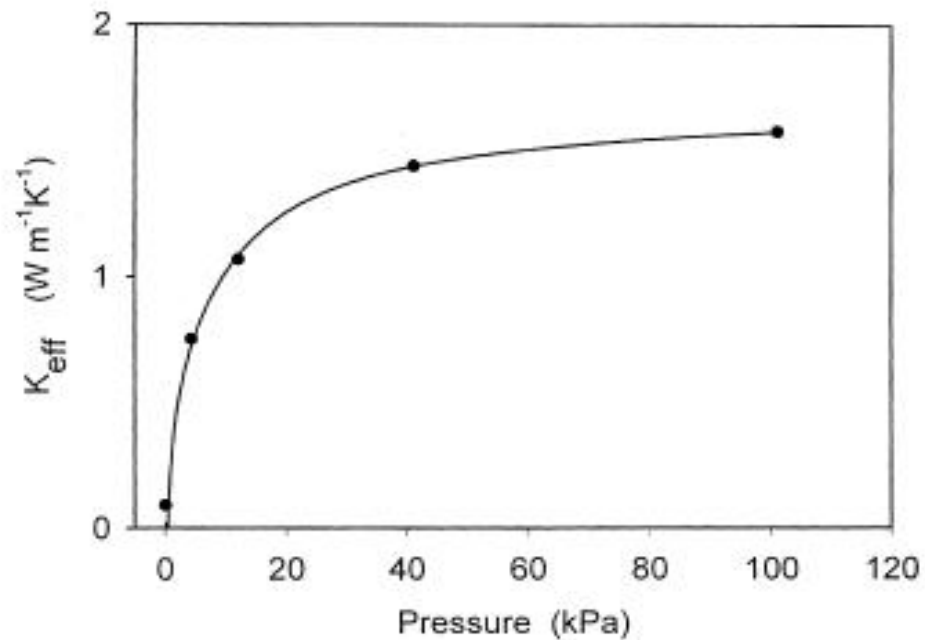
$$G_r = \frac{4\sigma_s}{2/\epsilon - 1} \alpha_r 4R^2 T^3, G_i = K_{gi} \alpha_i \pi B^2 / g,$$

$$G_o = K_g [1 - \exp(-R/\lambda)] \alpha_o \pi (R^2 - B^2) / R$$

$$\approx K_g [1 - \exp(-R/\lambda)] \alpha_o \pi R.$$

# Granular media (2)

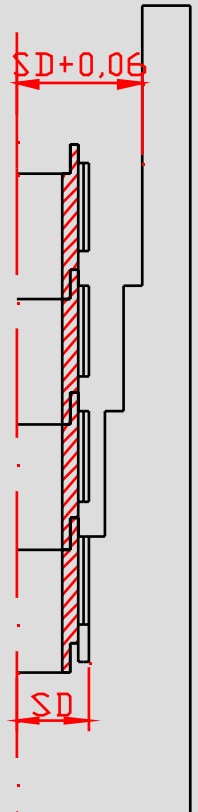
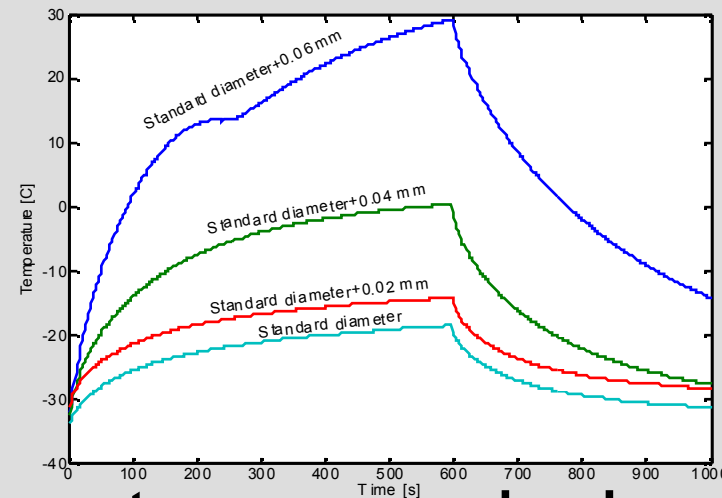
Slavin et al., 1 mm aluminum spheres



When the parameters of cometary/asteroid analogues are used then  $K \approx 0.2 \text{ W/m/K}$  at atmospheric pressure

# Future research

- Different sensor designs should be tested
- Modeling needs improvement => granularity of medium taken into account
- Thermal resistance between the sensors and the medium is the main experimental problem



- Between not too frequent space missions most of the planetary research will be done in the lab

Thank you for your attention